

# Solving the time dependent Ginzburg-Landau equation using COMSOL Multiphysics

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- 1 Ginzburg-Landau theory
- 2 Review of numerical simulations of TDGL equation
- 3 TDGL equation in COMSOL
- 4 PDE simulation flowchart

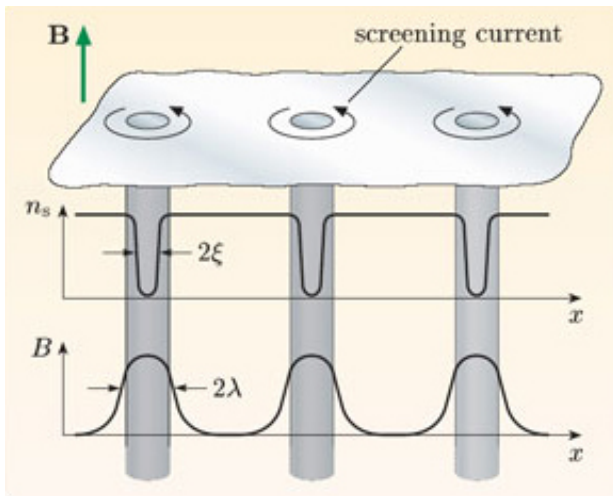
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## Type-II superconductors



Superconductivity at [open.edu](https://open.edu)

## The time dependent Ginzburg-Landau (TDGL) equation

$$\frac{\partial \Psi}{\partial t} = - \left( \frac{i}{\kappa} \nabla + \mathbf{A} \right)^2 \Psi + \Psi - |\Psi|^2 \Psi \quad (1)$$

$$\sigma \frac{\partial \mathbf{A}}{\partial t} = \frac{1}{2i\kappa} (\Psi^* \nabla \Psi - \Psi \nabla \Psi^*) - |\Psi|^2 \mathbf{A} - \nabla \times (\nabla \times \mathbf{A} - \mathbf{B}_a) \quad (2)$$

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## Boundary conditions

$$\nabla \Psi \cdot \mathbf{n} = 0, \quad \text{on } \partial\Omega \quad (3)$$

$$\nabla \times \mathbf{A} = \mathbf{B}_a, \quad \text{on } \partial\Omega \quad (4)$$

$$\mathbf{A} \cdot \mathbf{n} = 0, \quad \text{on } \partial\Omega \quad (5)$$

T.S. Alstrøm et al. Acta Appl. Math 115 (2011) 63

# Numerical solution of TDGLE

## Finite difference approximation

- W.D. Gropp et al. *J. Comp. Phys.*, 123 (1996) 254.
- M.V. Milošević, *Physica C*, 470 (2010) 791.
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JOURNAL OF COMPUTATIONAL PHYSICS 123, 254–266 (1996)  
ARTICLE NO. 0022

## Numerical Simulation of Vortex Dynamics in Type-II Superconductors\*

WILLIAM D. GROPP, HANS G. KAPER, GARY K. LEAF, DAVID M. LEVINE, MARIO PALUMBO, AND VALERIE M. VENOKUR

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Received November 14, 1994; revised April 10, 1995

This article describes the results of several numerical simulations of vortex dynamics in type-II superconductors. The underlying mathematical model is the time-dependent Ginzburg-Landau model. The simulations concern vortex penetration in the presence of twin boundaries, interface patterns between regions of opposite vortex orientation, and magnetic-flux entry patterns in superconducting samples. © 1996 Academic Press, Inc.

### 1. GINZBURG-LANDAU MODEL

In this article we report on several numerical simulations of vortex motion in type-II superconducting materials [1, 2]. The simulations are based on the time-dependent Ginzburg-Landau (TDGL) equations,

$$\mathbf{J}_s = \frac{e\hbar}{2m_s} (\phi^* \nabla \phi - \phi \nabla \phi^*) - \frac{e^2}{m_s c} |\phi|^2 \mathbf{A}, \quad (1.4)$$

The superscript  $*$  denotes complex conjugation,  $e$  is the “effective charge” of a superelectron ( $e_s < 0$ ), and  $m_s$  its “effective mass.” The constant  $D$  is a phenomenological diffusion coefficient. If  $\mathbf{J}$  is viewed as the sum of a “normal” current, which satisfies Ohm’s law, and the supercurrent,  $\sigma$  may be interpreted as the “coefficient of normal conductivity.”

The quantities  $a$  and  $b$  in (1.3) are phenomenological parameters; they are functions of external parameters, such as the temperature  $T$ , the concentration of impurities, etc.;  $b > 0$  for all  $T$ , and  $a$  changes sign at  $T_c$  ( $a < 0$  for  $T < T_c$ ,  $a > 0$  for  $T > T_c$ ).

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### The Ginzburg–Landau theory in application

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#### ARTICLE INFO

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#### ABSTRACT

A numerical approach to Ginzburg–Landau (GL) theory is demonstrated and we review its applications to several examples of current interest in the research on superconductivity. This analysis also shows the applicability of the two-dimensional approach to thin superconductors and the  $m$ -defined effective GL parameter  $\kappa$ . For two-gap superconductors, the conveniently written GL equations directly show that the magnetic behavior of the sample depends not just on the GL parameter of two bands, but also on the ratio of respective coherence lengths.

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#### 1. Introduction

Wherever a new scientific discovery is made, researchers must strive to explain it theoretically. In the case of superconductivity, it took more than two decades after its experimental discovery before the London theory was developed [1]. However, the London theory treats vortices as point-like objects and does not take into account the finite size and the inner structure of the vortices. In 1950, Landau and Ginzburg [2] developed a phenomenological theory, which combined Landau's theory of second-order phase transitions with a Schrödinger-like wave equation. Over the past 50 years, this theory had great success in explaining macroscopic properties of superconductors (such as the division of superconductors into two categories now referred to as type-I and type-II, and the description of the mixed state of type-II superconductors [3]), but it was also immensely useful for description of mesoscopic superconducting samples [4,5]. Even the full, microscopic Bardeen, Cooper, and Schrieffer (BCS) theory of superconductivity reduces to the Ginzburg–Landau (GL) theory close to the critical temperature  $T_c$ .

where  $\kappa$  is the GL parameter given as a ratio of magnetic penetration depth  $\lambda$  and the coherence length  $\xi$ , and  $H_0$  denotes the applied magnetic field. Eq. (1) is given in dimensionless form, where all distances are measured in units of  $\xi$ , the vector potential  $\tilde{A}$  in units of  $2\pi\phi_0/c$ , the magnetic field  $\tilde{H}$  in units of  $H_0 = \phi_0/2\pi\xi^2$ , and the order parameter  $\psi$  in units of  $\psi_0 = \sqrt{\phi_0/2\pi\xi}$ , with  $\alpha$  and  $\beta$  being the material-dependent coefficients.

Every part of Eq. (1) describes some physical property. In principle, it is possible to introduce some extra terms in the energy functional in order to describe the superconducting state deeper in the superconducting phase (see, for example, Ref. [6]), but the achieved corrections are very small and are rarely considered. The first part of Eq. (1) is the expansion of the energy difference between the superconducting and normal state for a homogeneous superconductor in the absence of an applied magnetic field<sup>1</sup> near the zero-field critical temperature  $T_c$ . The coefficient  $\alpha$  is a negative and changes sign as temperature is increased over  $T_{c0} = (T_c - T_{c0})$ , while  $\beta$  is a positive constant, independent of temperature. Therefore, the Cooper-pair density corresponding to temperature below  $T_c$  is in the absence of magnetic field to  $\psi = \sqrt{\alpha/\beta}$ .

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JOURNAL OF MATHEMATICAL PHYSICS 46, 095109 (2005)

### Numerical approximations of the Ginzburg-Landau models for superconductivity

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University Park, Pennsylvania 16802*

(Received 16 May 2005; accepted 17 May 2005; published online 29 September 2005)

In this paper, we review various methods for the numerical approximations of the Ginzburg-Landau models of superconductivity. Particular attention is given to the different treatment of gauge invariance in both the finite element, finite difference, and finite volume settings. Representative theoretical results, typical numerical simulations, and computational challenges are presented. Generalizations to other relevant models are also discussed. © 2005 American Institute of Physics.  
[DOI: 10.1063/1.2012127]

### 1. INTRODUCTION

The macroscopic model of Ginzburg and Landau<sup>1,2</sup> has been widely used to study both low-temperature and high-temperature superconductors. Due to its highly nonlinear nature, the complex energy landscape and the exotic dynamic responses of its solution to external conditions, its numerical simulations have become valuable tools in order to better understand the properties of the Ginzburg-Landau (GL) models and to provide further theoretical insight into the intriguing superconductivity phenomena.

The development of approximation methods of the Ginzburg-Landau model goes back to the

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## Finite Element Methods for the Time-Dependent Ginzburg-Landau Model of Superconductivity

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Department of Mathematics, Michigan State University  
East Lansing, MI 48824, U.S.A.

(Received and accepted April 1989)

**Abstract**—The initial-boundary value problem for the time-dependent Ginzburg-Landau equations that model the macroscopic behavior of superconductors is considered. The convergence of finite-dimensional, semidiscrete Galerkin approximations is studied as is a fully-discrete scheme. The results of some computational experiments are presented.

**Keywords**—Superconductivity, Time-dependent Ginzburg-Landau equations, Finite element methods.

### 1. THE TIME-DEPENDENT GINZBURG-LANDAU EQUATIONS

The steady state Ginzburg-Landau model for superconductivity (see, e.g., [1] or [2]) was extended to the time-dependent case by Gor'kov and Eliashberg in [3]. The latter model is defined by the differential equations

$$\eta \frac{\partial \psi}{\partial t} + i\eta \kappa \Phi \psi + \left( \frac{i}{\kappa} \nabla + \mathbf{A} \right)^2 \psi - \psi + |\psi|^2 \psi = 0, \quad \text{in } \Omega \times [0, T], \quad (1.1)$$

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Acta Appl Math (2011) 115:63–74  
DOI 10.1007/s10440-010-9580-8

## Magnetic Flux Lines in Complex Geometry Type-II Superconductors Studied by the Time Dependent Ginzburg-Landau Equation

Tommy Sonne Alstrøm · Mads Peter Sørensen ·  
Niels Falsig Pedersen · Søren Madsen

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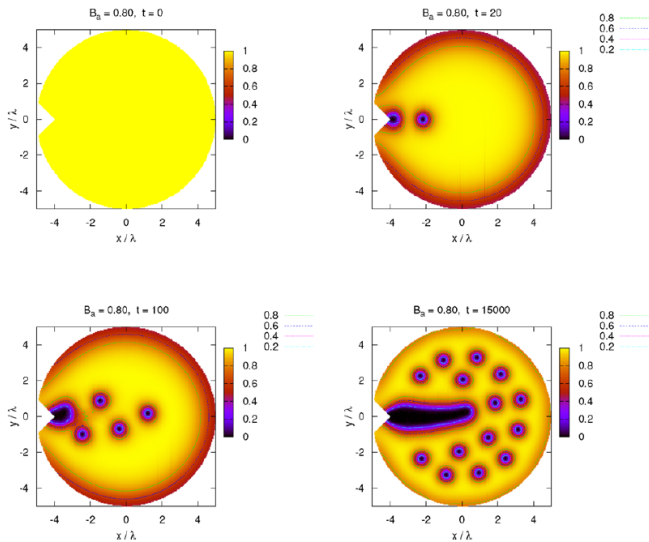
**Abstract** The time-dependent Ginzburg-Landau equation is solved numerically for type-II superconductors of complex geometry using the finite element method. The geometry has a marked influence on the magnetic vortex distribution and the vortex dynamics. We have observed generation of giant vortices at boundary defects, suppressing the superconducting state far into the superconductor.

**Keywords** Type II superconductivity · Ginzburg-Landau equation · Vortex lattices · Giant vortices

### 1 Introduction

In 1950 V.L. Ginzburg and L.D. Landau proposed a phenomenological theory for superconducting phase transitions [1]. The theory is based on a Schrödinger equation with a  $\phi^4$  potential and a kinetic term involving the momentum operator. For type-II superconductors the Ginzburg-Landau equation models the magnetic field penetration through quantized current vortices as the externally applied magnetic field exceeds a threshold value. A number

## Vortex dynamics in type-II superconductors



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# General form PDE interface

## General form PDE

$$e_a \frac{\partial^2 u}{\partial t^2} + d_a \frac{\partial u}{\partial t} + \nabla \cdot \Gamma = F$$

## General form PDE interface

## General form PDE

$$e_a \frac{\partial^2 \mathbf{u}}{\partial t^2} + d_a \frac{\partial \mathbf{u}}{\partial t} + \nabla \cdot \boldsymbol{\Gamma} = \mathbf{F}$$

## Dirichlet boundary conditions

$$\mathbf{R} = \mathbf{0}, \text{ on } \Omega$$

$$\mathbf{R} = \mathbf{R}(x, y, t, \mathbf{u}, \mathbf{u}_x, \mathbf{u}_y)$$

## General form PDE interface

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$$\mathbf{R} = \mathbf{R}(x, y, t, \mathbf{u}, \mathbf{u}_x, \mathbf{u}_y)$$

## Neumann boundary conditions

$$-\mathbf{n} \cdot \boldsymbol{\Gamma} = \mathbf{G} + \left( \frac{\partial \mathbf{R}}{\partial \mathbf{u}} \right)^T \cdot \boldsymbol{\mu}, \text{ on } \Omega$$

$$\boldsymbol{\Gamma} = \boldsymbol{\Gamma}(x, y, t, \mathbf{u}, \mathbf{u}_x, \mathbf{u}_y), \mathbf{G} = \mathbf{G}(x, y, t, \mathbf{u}, \mathbf{u}_x, \mathbf{u}_y)$$

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## Zero flux

$$-\mathbf{n} \cdot \boldsymbol{\Gamma} = 0, \text{ on } \Omega$$

## Notation

$$\Psi = \begin{pmatrix} u_1 \\ u_2 \end{pmatrix}, \quad \nabla = \begin{pmatrix} \partial_x & \partial_y \end{pmatrix}, \quad \mathbf{A} = \begin{pmatrix} u_3 \\ u_4 \end{pmatrix}$$

The Eq. (1)  $\frac{\partial \Psi}{\partial t} = - \left( \frac{i}{\kappa} \nabla + \mathbf{A} \right)^2 \Psi + \Psi - |\Psi|^2 \Psi$  we can rewrite as:

$$\partial_t \begin{pmatrix} u_1 \\ u_2 \end{pmatrix} = - \left( \frac{i}{\kappa} \nabla + A \right)^2 \begin{pmatrix} u_1 \\ u_2 \end{pmatrix} + \begin{pmatrix} u_1 \\ u_2 \end{pmatrix} - (u_1^2 + u_2^2) \begin{pmatrix} u_1 \\ u_2 \end{pmatrix}$$

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$$\partial_t u_1 = \nabla \cdot \begin{pmatrix} u_{1x}/\kappa^2 \\ u_{1y}/\kappa^2 \end{pmatrix} + \frac{1}{\kappa} (u_{3x} + u_{4y}) u_2 + \frac{2}{\kappa} (u_3 u_{2x} + u_4 u_{2y}) - (u_3^2 + u_4^2) u_1 + u_1 - (u_1^2 + u_2^2) u_1$$

$$\partial_t u_2 = \nabla \cdot \begin{pmatrix} u_{2x}/\kappa^2 \\ u_{2y}/\kappa^2 \end{pmatrix} - \frac{1}{\kappa} (u_{3x} + u_{4y}) u_1 - \frac{2}{\kappa} (u_3 u_{1x} + u_4 u_{1y}) - (u_3^2 + u_4^2) u_2 + u_2 - (u_1^2 + u_2^2) u_2$$

$$\partial_t u_1 + \nabla \cdot \underbrace{\begin{pmatrix} -u_{1x}/\kappa^2 \\ -u_{1y}/\kappa^2 \end{pmatrix}}_{\Gamma_1} = F_1$$

$$F_1 = -\frac{1}{\kappa} (u_{3x} + u_{4y}) u_1 - \frac{2}{\kappa} (u_3 u_{1x} + u_4 u_{1y}) - (u_3^2 + u_4^2) u_2$$

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$$\partial_t u_2 + \nabla \cdot \underbrace{\begin{pmatrix} -u_{2x}/\kappa^2 \\ -u_{2y}/\kappa^2 \end{pmatrix}}_{\Gamma_2} = F_2$$

$$F_2 = -(u_3^2 + u_4^2) u_2 - \frac{1}{\kappa} ((u_{3x} + u_{4y}) u_2 + u_3 u_{1x} + u_4 u_{1y}) + u_2 - (u_1^2 + u_2^2) u_2$$

$$\partial_t u_1 + \nabla \cdot \underbrace{\begin{pmatrix} -u_{1x}/\kappa^2 \\ -u_{1y}/\kappa^2 \end{pmatrix}}_{\Gamma_1} = F_1$$

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$$F_2 = -(u_3^2 + u_4^2) u_2 - \frac{1}{\kappa} ((u_{3x} + u_{4y}) u_2 + u_3 u_{1x} + u_4 u_{1y}) + u_2 - (u_1^2 + u_2^2) u_2$$

$$\nabla \Psi \cdot \mathbf{n} = 0 \quad \equiv \quad -\mathbf{n} \cdot \mathbf{\Gamma} = 0$$

The Eq. (2)  $\sigma \frac{\partial \mathbf{A}}{\partial t} = \frac{1}{2i\kappa} (\Psi^* \nabla \Psi - \Psi \nabla \Psi^*) - |\Psi|^2 \mathbf{A} - \nabla \times (\nabla \times \mathbf{A} - \mathbf{B}_a)$  we can rewrite as:

$$\begin{aligned}\sigma \partial_t u_3 &= (u_1 u_{2x} - u_2 u_{1x}) / \kappa - (u_1^2 + u_2^2) u_3 - \nabla \cdot (0, u_{4x} - u_{3y} - B_{az})^T \\ \sigma \partial_t u_4 &= (u_1 u_{2y} - u_2 u_{1y}) / \kappa - (u_1^2 + u_2^2) u_3 - \nabla \cdot (-u_{4x} + u_{3y} + B_{az}, 0)^T\end{aligned}$$

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$$\begin{aligned}\sigma \partial_t u_3 &= (u_1 u_{2x} - u_2 u_{1x})/\kappa - (u_1^2 + u_2^2)u_3 - \nabla \cdot (0, u_{4x} - u_{3y} - B_{az})^T \\ \sigma \partial_t u_4 &= (u_1 u_{2y} - u_2 u_{1y})/\kappa - (u_1^2 + u_2^2)u_3 - \nabla \cdot (-u_{4x} + u_{3y} + B_{az}, 0)^T\end{aligned}$$

$$\begin{aligned}\sigma \partial_t u_3 + \nabla \cdot \underbrace{(0, u_{4x} - u_{3y} - B_{az})^T}_{\Gamma_3} &= \underbrace{(u_1 u_{2x} - u_2 u_{1x})/\kappa - (u_1^2 + u_2^2)u_3}_{F_3} \\ \sigma \partial_t u_4 + \nabla \cdot \underbrace{(-u_{4x} + u_{3y} + B_{az}, 0)^T}_{\Gamma_4} &= \underbrace{(u_1 u_{2y} - u_2 u_{1y})/\kappa - (u_1^2 + u_2^2)u_3}_{F_4}\end{aligned}$$

The Eq. (2)  $\sigma \frac{\partial \mathbf{A}}{\partial t} = \frac{1}{2i\kappa} (\Psi^* \nabla \Psi - \Psi \nabla \Psi^*) - |\Psi|^2 \mathbf{A} - \nabla \times (\nabla \times \mathbf{A} - \mathbf{B}_a)$  we can rewrite as:

$$\begin{aligned}\sigma \partial_t u_3 &= (u_1 u_{2x} - u_2 u_{1x})/\kappa - (u_1^2 + u_2^2)u_3 - \nabla \cdot (0, u_{4x} - u_{3y} - B_{az})^T \\ \sigma \partial_t u_4 &= (u_1 u_{2y} - u_2 u_{1y})/\kappa - (u_1^2 + u_2^2)u_3 - \nabla \cdot (-u_{4x} + u_{3y} + B_{az}, 0)^T\end{aligned}$$

$$\begin{aligned}\sigma \partial_t u_3 + \nabla \cdot \underbrace{(0, u_{4x} - u_{3y} - B_{az})^T}_{\Gamma_3} &= \underbrace{(u_1 u_{2x} - u_2 u_{1x})/\kappa - (u_1^2 + u_2^2)u_3}_{F_3} \\ \sigma \partial_t u_4 + \nabla \cdot \underbrace{(-u_{4x} + u_{3y} + B_{az}, 0)^T}_{\Gamma_4} &= \underbrace{(u_1 u_{2y} - u_2 u_{1y})/\kappa - (u_1^2 + u_2^2)u_3}_{F_4}\end{aligned}$$

$$\nabla \times \mathbf{A} = \mathbf{B}_a \quad \equiv \quad -\mathbf{n} \cdot \mathbf{\Gamma} = 0$$

How to implement the boundary condition:

$$\mathbf{A} \cdot \mathbf{n} = 0, \quad \text{on } \partial\Omega ?$$

How to implement the boundary condition:

$$\mathbf{A} \cdot \mathbf{n} = 0, \quad \text{on } \partial\Omega ?$$

Use dummy function  $u_5!!!$

How to implement the boundary condition:

$$\mathbf{A} \cdot \mathbf{n} = 0, \quad \text{on } \partial\Omega ?$$

Use dummy function  $u_5$ !!!

$$\underbrace{\nabla \cdot \begin{pmatrix} u_3 \\ u_4 \end{pmatrix}}_{\Gamma_5} = \underbrace{u_{3x} + u_{4y} + u_5}_{F_5}$$

## TDGLE in COMSOL

$$\mathbf{e}_a \frac{\partial^2 \mathbf{u}}{\partial t^2} + \mathbf{d}_a \frac{\partial \mathbf{u}}{\partial t} + \nabla \cdot \boldsymbol{\Gamma} = \mathbf{F}$$

$$\mathbf{e}_a = \mathbf{0}, \mathbf{d}_a = \text{diag} \{1, 1, \sigma, \sigma, 0\}$$

$$\boldsymbol{\Gamma} = \begin{pmatrix} (-u_{1x}/\kappa^2, -u_{1y}/\kappa^2)^T \\ (-u_{2x}/\kappa^2, -u_{2y}/\kappa^2)^T \\ (0, u_{4x} - u_{3y} - B_{az})^T \\ (-u_{4x} + u_{3y} + B_{az}, 0)^T \\ (u_3, u_4)^T \end{pmatrix}, \quad \mathbf{F} = \begin{pmatrix} F_1 \\ F_2 \\ (u_1 u_{2x} - u_2 u_{1x})/\kappa - (u_1^2 + u_2^2)u_3 \\ (u_1 u_{2y} - u_2 u_{1y})/\kappa - (u_1^2 + u_2^2)u_3 \\ u_{3x} + u_{4y} + u_5 \end{pmatrix}$$

## TDGLE in COMSOL

$$e_a \frac{\partial^2 u}{\partial t^2} + d_a \frac{\partial u}{\partial t} + \nabla \cdot \Gamma = F$$

$$e_a = 0, d_a = \text{diag} \{1, 1, \sigma, \sigma, 0\}$$

$$\Gamma = \begin{pmatrix} (-u_{1x}/\kappa^2, -u_{1y}/\kappa^2)^T \\ (-u_{2x}/\kappa^2, -u_{2y}/\kappa^2)^T \\ (0, u_{4x} - u_{3y} - B_{az})^T \\ (-u_{4x} + u_{3y} + B_{az}, 0)^T \\ (u_3, u_4)^T \end{pmatrix}, \quad F = \begin{pmatrix} F_1 \\ F_2 \\ (u_1 u_{2x} - u_2 u_{1x})/\kappa - (u_1^2 + u_2^2)u_3 \\ (u_1 u_{2y} - u_2 u_{1y})/\kappa - (u_1^2 + u_2^2)u_3 \\ u_{3x} + u_{4y} + u_5 \end{pmatrix}$$

Zero flux

$$-\mathbf{n} \cdot \Gamma = 0, \text{ on } \Omega$$

## TDGLE in COMSOL

$$e_a \frac{\partial^2 u}{\partial t^2} + d_a \frac{\partial u}{\partial t} + \nabla \cdot \Gamma = F$$

$$e_a = 0, d_a = \text{diag} \{1, 1, \sigma, \sigma, 0\}$$

$$\Gamma = \begin{pmatrix} (-u_{1x}/\kappa^2, -u_{1y}/\kappa^2)^T \\ (-u_{2x}/\kappa^2, -u_{2y}/\kappa^2)^T \\ (0, u_{4x} - u_{3y} - B_{az})^T \\ (-u_{4x} + u_{3y} + B_{az}, 0)^T \\ (u_3, u_4)^T \end{pmatrix}, \quad F = \begin{pmatrix} F_1 \\ F_2 \\ (u_1 u_{2x} - u_2 u_{1x})/\kappa - (u_1^2 + u_2^2)u_3 \\ (u_1 u_{2y} - u_2 u_{1y})/\kappa - (u_1^2 + u_2^2)u_3 \\ u_{3x} + u_{4y} + u_5 \end{pmatrix}$$

Zero flux

$$-\mathbf{n} \cdot \Gamma = 0, \text{ on } \Omega$$

Initial conditions

$$u_1 = 1, \quad u_2 = 0, \quad u_3 = 0, \quad u_4 = 0, \quad u_5 = 0$$

# PDE simulation flowchart

- 1 Model initialization
- 2 Global and local definitions
- 3 Geometry settings
- 4 PDE interface settings
- 5 Mesh generation
- 6 PDE solution
- 7 Postprocessing

# PDE simulation flowchart

- ❶ Model initialization
- ❷ Global and local definitions
- ❸ Geometry settings
- ❹ PDE interface settings
- ❺ Mesh generation
- ❻ PDE solution
- ❼ Postprocessing

# PDE simulation flowchart

- 1 Model initialization
- 2 Global and local definitions
- 3 Geometry settings
- 4 PDE interface settings
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# PDE simulation flowchart

- 1 Model initialization
- 2 Global and local definitions
- 3 **Geometry settings**
- 4 PDE interface settings
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# PDE simulation flowchart

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# PDE simulation flowchart

- 1 Model initialization
- 2 Global and local definitions
- 3 Geometry settings
- 4 PDE interface settings
- 5 Mesh generation
- 6 PDE solution
- 7 Postprocessing

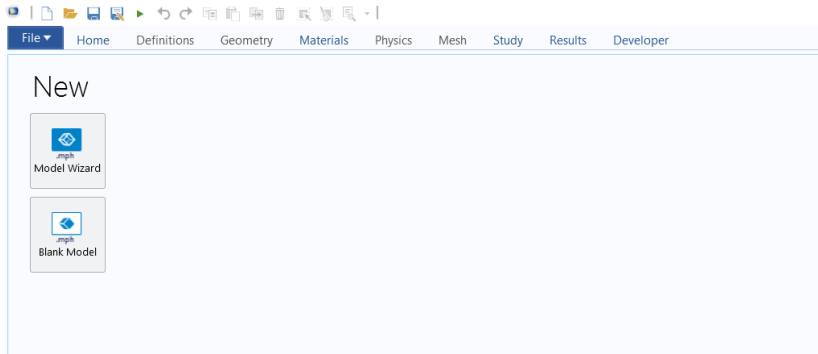
# PDE simulation flowchart

- ① Model initialization
- ② Global and local definitions
- ③ Geometry settings
- ④ PDE interface settings
- ⑤ Mesh generation
- ⑥ PDE solution
- ⑦ Postprocessing

# PDE simulation flowchart

- ① Model initialization
- ② Global and local definitions
- ③ Geometry settings
- ④ PDE interface settings
- ⑤ Mesh generation
- ⑥ PDE solution
- ⑦ Postprocessing

# Model initialization



Untitled.mph - COMSOL Multi

File Home Definitions Geometry Materials Physics Mesh Study Results Developer

## Select Physics

- ▶ Recently Used
- ▶ AC/DC
- ▶ Acoustics
- ▶ Chemical Species Transport
- ▶ Electrochemistry
- ▶ Fluid Flow
- ▶ Heat Transfer
- ▶ Optics
- ▶ Plasma
- ▶ Radio Frequency
- ▶ Semiconductor
- ▶ Structural Mechanics
- ▶ Mathematics

## Recently Used

Under this node you can conveniently access a few of the most recently used physics interfaces.

## Select Physics

Search

- Recently Used
- AC/DC
- Acoustics
- Chemical Species Transport
- Electrochemistry
- Fluid Flow
- Heat Transfer
- Optics
- Plasma
- Radio Frequency
- Semiconductor
- Structural Mechanics
- Mathematics
  - PDE Interfaces
    - Coefficient Form PDE (c)
    - General Form PDE (g)**
    - Wave Form PDE (wahw)
    - Weak Form PDE (w)
    - PDE, Boundary Elements (pdebe)
  - Lower Dimensions
  - ODE and DAE Interfaces
  - Optimization and Sensitivity
  - Classical PDEs
  - Muxin Interface

Add

Added physics interfaces:

- General Form PDE (g)

Remove

← Space Dimension

→ Study

Help

Cancel

Done

## General Form PDE

The General Form PDE interface provides a general interface for specifying and solving PDEs in the general form. The format, using the divergence of a flux vector, is closely related to the conservation laws that govern many areas of physics. In practical applications, the flux vector typically represents the flux of a conserved quantity such as heat, charge, mass, or momentum. This flux is usually related in some empirical way, via a material law, to the gradient of the dependent variable.

## Select Physics

Search

- ▷ Recently Used
- ▷ AC/DC
- ▷ Acoustics
- ▷ Chemical Species Transport
- ▷ Electrochemistry
- ▷ Fluid Flow
- ▷ Heat Transfer
- ▷ Optics
- ▷ Plasma
- ▷ Radio Frequency
- ▷ Semiconductor
- ▷ Structural Mechanics
- ▲ Δu Mathematics
  - ▲ Δu PDE Interfaces
    - Δu Coefficient Form PDE (c)
    - Δu General Form PDE (g)**
    - Δu Wave Form PDE (wahw)
    - f-w Weak Form PDE (w)
    - Δu PDE, Boundary Elements (pdebe)
    - ▷ Δu Lower Dimensions
    - ▷  $\frac{d}{dt}$  ODE and DAE Interfaces
    - ▷ Optimization and Sensitivity
    - ▷  $\nabla^2$  Classical PDEs
    - ▷ Moving Interface

Add

Added physics interfaces:

Δu General Form PDE (g)

Remove

## Review Physics Interface

General Form PDE (g)

### Dependent Variables

Field name:

Number of dependent variables:

Dependent variables:

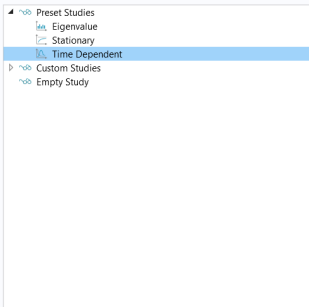
u1
u2
u3
u4
u5

+
-

### Units

» Dependent variable quantity	Unit	
Dimensionless	1	
» Source term quantity	Unit	
Custom unit	1	

## Select Study



Added study:

Time Dependent

Added physics interfaces:

General Form PDE (g)

Physics



Help



Cancel



Done

## Time Dependent

The Time Dependent study is used when field variables change over time.

Examples: In electromagnetics, it is used to compute transient electromagnetic fields, including electromagnetic wave propagation in the time domain. In heat transfer, it is used to compute temperature changes over time. In solid mechanics, it is used to compute the time-varying deformation and motion of solids subject to transient loads. In acoustics, it is used to compute the time-varying propagation of pressure waves. In fluid flow, it is used to compute unsteady flow and pressure fields. In chemical species transport, it is used to compute chemical composition over time. In chemical reactions, it is used to compute the reaction kinetics and the chemical composition of a reacting system.

# Global and local definitions

Model Builder

Settings Properties

Parameters

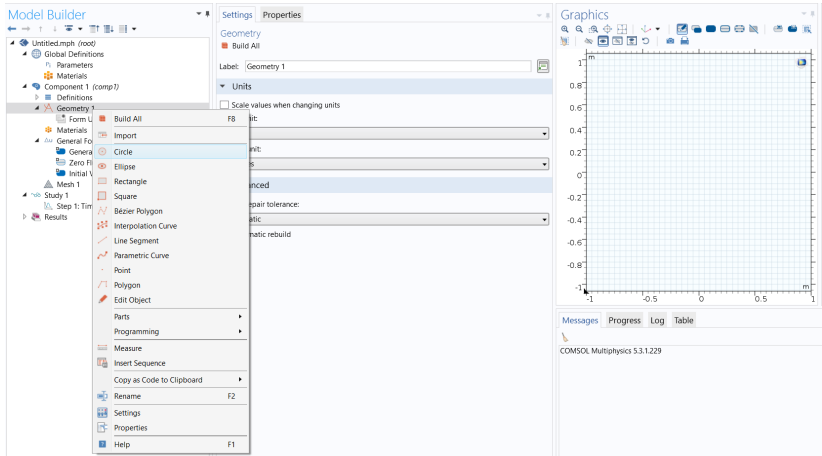
Parameters

Name	Expression	Value	Description
Lx	10	10	
Ly	10	10	
kappa	4	4	
Baz	0.8	0.8	
sigma	1	1	
R	4	4	

Model Builder tree structure:

- Untitled.mph (root)
  - Global Definitions
    - Parameters
  - Component 1 (comp1)
    - Definitions
    - Geometry 1
      - Materials
    - General Form PDE (g)
      - General Form PDE 1
      - Zero Flux 1
      - Initial Values 1
    - Mesh 1
  - Study 1
    - Step 1: Time Dependent
  - Results

## Geometry settings



**Model Builder**

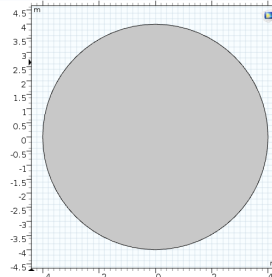
- Untitled.mph (root)
  - Global Definitions
    - Parameters
    - Materials
  - Component 1 (comp1)
    - Definitions
    - Geometry 1
      - Circle 1 (c1)
        - Form Union (fin)
        - Materials
      - General Form PDE (gp)
        - General Form PDE 1
        - Zero Flux 1
        - Initial Values 1
      - Mesh 1
    - Study 1
      - Step 1: Time Dependent
      - Results

**Settings** Properties

**Circle**

- Build Selected Build All Objects
- Label: Circle 1
- Object Type
  - Type: Solid
- Size and Shape
  - Radius: R m
  - Sector angle: 360 deg
- Position
  - Base: Center
  - x: 0 m
  - y: 0 m
- Rotation Angle
  - Rotation: 0 deg
- Layers
- Selections of Resulting Entities
  - Contribute to: None New
  - ☐ Resulting objects selection
  - Show in physics: Domain selection

**Graphics**



Messages Progress Log Table

COMSOL Multiphysics 5.3.1.229

**Model Builder**

- GL\_disk.mph (root)
  - Global Definitions
    - Parameters
  - Materials
    - Component 1 (comp1)
      - Definitions
      - Geometry 1
        - Circle 1 (c1)
        - Bézier Polygon 1 (b1)**
        - Form Union (fn)
  - Materials
    - General Form PDE (g)
      - General Form PDE 1
      - Zero Flux 1
      - Initial Values 1
  - Mesh 1
  - Study 1
    - Step 1: Time Dependent
  - Results

**Settings** | **Properties**

**Bézier Polygon**

Build Selected | Build All Objects

**General**

Type: Solid

**Polygon Segments**

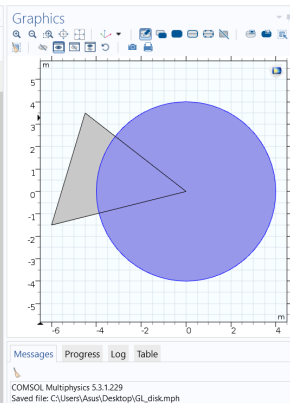
Added segments

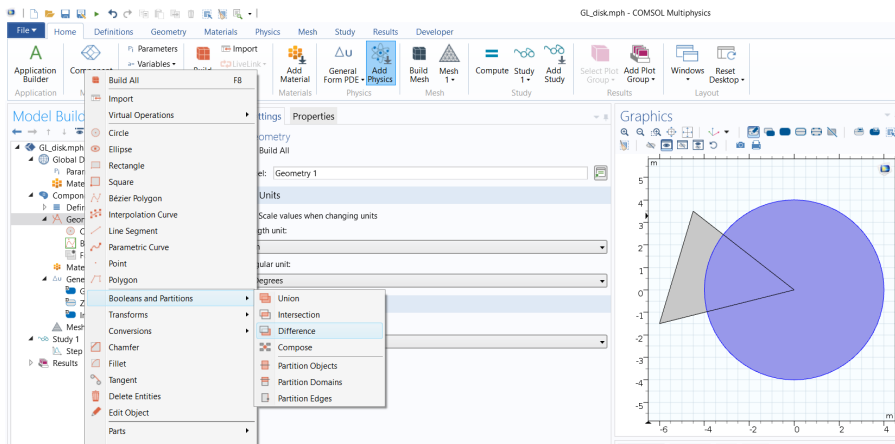
- Segment 1 (linear)
- Segment 2 (linear)
- Segment 3 (linear)

Add Linear | Add Quadratic | Add Cubic | Delete

Control points

	x	y	
1	0	0	m
2	-4.5	3.5	m





## Model Builder

- GL\_disk.mph (root)
  - Global Definitions
    - Parameters
    - Materials
  - Component 1 (comp1)
    - Definitions
      - Geometry 1
        - Circle 1 (c1)
        - Bézier Polygon 1 (b1)
        - Difference 1 (dif1)
        - Form Union (fn)
      - Materials
    - General Form PDE (g)
      - General Form PDE 1
      - Zero Flux 1
      - Initial Values 1
    - Mesh 1
  - Study 1
    - Step 1: Time Dependent
    - Results

## Settings

## Properties

## Difference

Build Selected Build All Objects

Label: Difference 1

## Difference

Objects to add:

☐ c1

Active

Objects to subtract:

☐ b1

Active

☐ Keep input objects

☒ Keep interior boundaries

Repair tolerance: Automatic

## Selections of Resulting Entities

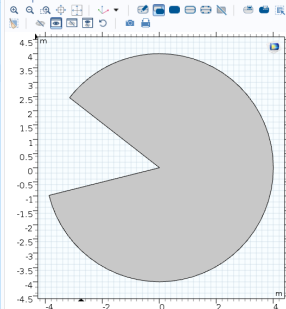
Contribute to: None

New

☐ Resulting objects selection

Show in physics: Domain selection

## Graphics



Messages Progress Log Table

COMSOL Multiphysics 5.3.1.229  
Saved file: C:\Users\Asus\Desktop\GL\_disk.mph

# PDE interface settings

**Model Builder**

- GL\_diskmph (root)
  - Global Definitions
    - Parameters
    - Materials
  - Component 1 (comp1)
    - Definitions
    - Geometry 1
      - Circle 1 (c1)
      - Bézier Polygon 1 (b1)
      - Difference 1 (dif1)
      - Form Union (fin)
    - Materials
      - General Form PDE (g)
        - General Form PDE 1**
        - Zero Flux 1
        - Initial Values 1
    - Mesh 1
    - Study 1
      - Step 1: Time Dependent
      - Results

**Settings** **Properties**

**General Form PDE**

**Domain Selection**

Selection: All domains

1

Active

**Override and Contribution**

**Equation**

Show equation assuming:

Study 1, Time Dependent

$$e_a \frac{\partial^2 \mathbf{u}}{\partial t^2} + d_a \frac{\partial \mathbf{u}}{\partial t} + \nabla \cdot \Gamma = \mathbf{f}$$

$$\mathbf{u} = [u_1, u_2, u_3, \dots, u_E]^T$$

$$\nabla = \left[ \frac{\partial}{\partial x}, \frac{\partial}{\partial y} \right]$$

**Conservative Flux**

-u1x/kappa^2	x	m
-u1y/kappa^2	y	m
-u2x/kappa^2	x	m
-u2y/kappa^2	y	m
0	x	m
u4x-u3y-Baz	y	m
-u4x+u3y+Baz	x	m
0	y	m
u3	x	m
u4	y	m

▼ Damping or Mass Coefficient

$d_a$	1	s	0	s	0	s	0	s	0	s
	0	s	1	s	0	s	0	s	0	s
	0	s	0	s	sigma	s	0	s	0	s
	0	s	0	s	0	s	sigma	s	0	s
	0	s	0	s	0	s	0	s	0	s

▼ Mass Coefficient

$e_a$	0	$s^2$	0	$s^2$	0	$s^2$	0	$s^2$	0	$s^2$
	0	$s^2$	0	$s^2$	0	$s^2$	0	$s^2$	0	$s^2$
	0	$s^2$	0	$s^2$	0	$s^2$	0	$s^2$	0	$s^2$
	0	$s^2$	0	$s^2$	0	$s^2$	0	$s^2$	0	$s^2$
	0	$s^2$	0	$s^2$	0	$s^2$	0	$s^2$	0	$s^2$

▷ Conservative Flux

▼ Source Term

$$(u_3x+u_4y)*u_2/kappa+2*(u_3*u_2x+u_4*u_2y)/kappa-(u_3^2+u_4^2)*u_1+u_1-(u_1^2+u_2^2)*u_1$$

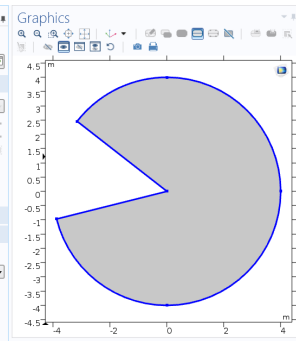
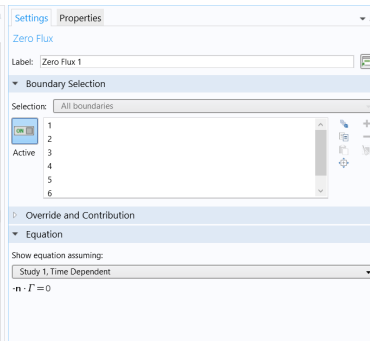
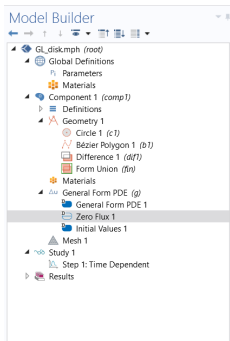
$$-(u_3x+u_4y)*u_1/kappa-2*(u_3*u_1x+u_4*u_1y)/kappa-(u_3^2+u_4^2)*u_2+u_2-(u_1^2+u_2^2)*u_2$$

$f$   $(u_1*u_2x-u_2*u_1x)/kappa-(u_1^2+u_2^2)*u_3$

$$(u_1*u_2y-u_2*u_1y)/kappa-(u_1^2+u_2^2)*u_4$$

$$u_3x+u_4y+u_5$$

▷ Damping or Mass Coefficient



- Component 1 (*comp1*)
  - Definitions
  - Geometry 1
    - Circle 1 (*c1*)
    - Bézier Polygon 1 (*b1*)
    - Difference 1 (*dif1*)
    - Form Union (*fin*)
  - Materials
  - General Form PDE (*g*)
    - General Form PDE 1
    - Zero Flux 1
    - Initial Values 1
  - Mesh 1
  - Study 1
    - Step 1: Time Dependent
  - Results

## Override and Contribution

## Initial Values

Initial value for u1:

 $u1$  1 1

Initial time derivative of u1:

 $\frac{\partial u1}{\partial t}$  0 1/s

Initial value for u2:

 $u2$  0 1

Initial time derivative of u2:

 $\frac{\partial u2}{\partial t}$  0 1/s

Initial value for u3:

 $u3$  0 1

Initial time derivative of u3:

 $\frac{\partial u3}{\partial t}$  0 1/s

Initial value for u4:

 $u4$  0 1

Initial time derivative of u4:

 $\frac{\partial u4}{\partial t}$  0 1/s

Initial value for u5:

 $u5$  0 1

Initial time derivative of u5:

 $\frac{\partial u5}{\partial t}$  0 1/s

# Mesh generation

The screenshot displays the COMSOL Multiphysics interface during the mesh generation process. The interface is divided into three main panels:

- Model Builder:** Located on the left, it shows a hierarchical tree of the model. The 'Mesh' node is selected under 'General Form PDE 1'. The tree includes 'Global Definitions', 'Parameters', 'Materials', 'Component 1 (comp1)', 'Definitions', 'Geometry 1' (containing 'Circle 1 (c1)', 'Bézier Polygon 1 (b1)', 'Difference 1 (d1f1)', and 'Form Union (fin)'), 'Materials', 'General Form PDE (g)' (containing 'General Form PDE 1', 'Zero Flux 1', and 'Initial Values 1'), 'Mesh 1', 'Study 1', and 'Step 1: Time Dependent'.
- Settings:** Located in the middle, it shows the 'Mesh' settings for 'Mesh 1'. The 'Sequence type' is set to 'Physics-controlled mesh' and the 'Element size' is set to 'Finer'.
- Graphics:** Located on the right, it shows a 2D plot of the mesh. The mesh is a triangular mesh covering a circular domain with a wedge-shaped cutout. The axes range from -4.5 to 4.5 meters.

# PDE solution

Model Builder

GL\_disk.mph (root)

- Global Definitions
  - Parameters
  - Materials
- Component 1 (comp1)
  - Definitions
  - Geometry 1
    - Circle 1 (c1)
    - Bézier Polygon 1 (b1)
    - Difference 1 (dif1)
    - Form Union (fin)
  - Materials
  - General Form PDE (g)
    - General Form PDE 1
    - Zero Flux 1
    - Initial Values 1
  - Mesh 1
- Study 1
  - Step 1: Time Dependent
  - Solver Configurations
  - Results
    - Data Sets
    - Derived Values
    - Tables

Settings Properties

Time Dependent

Compute (F8) Update Solution

Label: Time Dependent

Study Settings

Time unit: s

Times: range(0,1,400) s

Tolerance: Physics controlled

Results While Solving

Physics and Variables Selection

☐ Modify model configuration for study step

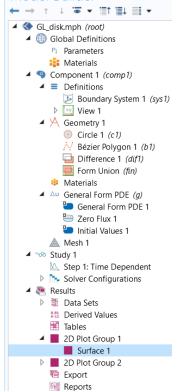
Physics interface	Solve for	Discretization
General Form PDE	<input checked="" type="checkbox"/>	Physics settings

Values of Dependent Variables

Mesh Selection

Study Extensions

## Model Builder



## Settings Properties

## Surface

Plot

Label: Surface 1

## Data

Data set: From parent

## Expression

Expression:

$u1^2 + u2^2$

Unit:

1

☐ Description:

$u1^2 + u2^2$

## Title

Title type: None

## Range

## Coloring and Style

Coloring: Color table

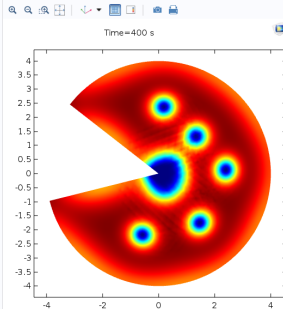
Color table: Rainbow

☒ Color legend

☐ Reverse color table

☐ Symmetrize color range

## Graphics Convergence Plot 1



## Messages Progress Log Table

Saved file: C:\Users\Asus\Desktop\GL\_disk.mph

Complete mesh consists of 473 domain elements and 57 boundary elements.

Complete mesh consists of 1541 domain elements and 103 boundary elements.

Saved file: C:\Users\Asus\Desktop\GL\_disk.mph

Number of degrees of freedom solved for: 1541. Color: 1541. Element: 1541.



# Parametric sweep

The screenshot shows the 'Model Builder' on the left and the 'Parametric Sweep' settings on the right.

**Model Builder (Left Panel):**

- GL\_disk.mph (root)
  - Global Definitions
    - Parameters
    - Materials
  - Component 1 (comp1)
    - Definitions
      - Boundary System 1 (sys1)
        - View 1
    - Geometry 1
      - Circle 1 (c1)
      - Bézier Polygon 1 (b1)
      - Difference 1 (dif1)
      - Form Union (fin)
    - Materials
      - General Form PDE (g)
        - General Form PDE 1
        - Zero Flux 1
        - Initial Values 1
    - Mesh 1
  - Study 1
    - Parametric Sweep**
    - Step 1: Time Dependent
    - Solver Configurations
    - Job Configurations
    - Results

**Parametric Sweep Settings (Right Panel):**

Settings Properties

Parametric Sweep

Compute Update Solution

Label: Parametric Sweep

**Study Settings**

Sweep type: Specified combinations

Parameter name	Parameter value list	Parameter unit
Baz	range(0, 0.1, 5)	

**Output While Solving**

☐ Plot

Plot group: 2D Plot Group 1

Probes: All

☐ Accumulated probe table

Output table: New

# Cooper pair density $|\psi|^2$ dependence on $B_a$

Thank you for attention!

# The time dependent Ginzburg-Landau (TDGL) equation

$$\frac{\hbar^2}{2mD} \left( \frac{\partial}{\partial t} + i \frac{q}{\hbar} \Phi \right) \Psi = - \frac{1}{2m} \left( \frac{\hbar}{i} \nabla - q \mathbf{A} \right)^2 \Psi + \alpha \Psi - \beta |\Psi|^2 \Psi$$

$$\sigma \left( \frac{\partial \mathbf{A}}{\partial t} + \nabla \Phi \right) = \frac{q \hbar}{2m i} (\Psi^* \nabla \Psi - \Psi \nabla \Psi^*) - \frac{q^2}{m} |\Psi|^2 \mathbf{A} - \frac{1}{\mu_0} \nabla \times (\nabla \times \mathbf{A} - \mathbf{B}_a)$$

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## Boundary conditions

$$\left( \frac{\hbar}{i} \nabla \Psi - q \mathbf{A} \Psi \right) \cdot \mathbf{n} = 0, \quad \text{on } \partial \Omega$$

$$\mathbf{B}_i = \mathbf{B}_a, \quad \text{on } \partial \Omega$$

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# Normalization

$$(x, y, z, t) = \left( \lambda x', \lambda y', \lambda z', \frac{\xi^2}{D} t' \right), \quad \mathbf{A} = \frac{\hbar}{q\xi} \mathbf{A}'$$

$$\Psi = \sqrt{\frac{\alpha}{\beta}} \Psi', \quad \Phi = \alpha D \kappa^2 \sqrt{\frac{2\mu_0}{b}} \Phi', \quad \sigma = \frac{1}{\mu_0 D \kappa^2} \sigma'$$

$$\left( \frac{\partial}{\partial t} + i\kappa\Phi \right) \Psi = - \left( \frac{i}{\kappa} \nabla + \mathbf{A} \right)^2 \Psi + \Psi - |\Psi|^2 \Psi$$

$$\sigma \left( \frac{\partial \mathbf{A}}{\partial t} + \nabla \Phi \right) = \frac{1}{2i\kappa} (\Psi^* \nabla \Psi - \Psi \nabla \Psi^*) - |\Psi|^2 \mathbf{A} - (\nabla \times \mathbf{A} - \mathbf{B}_a)$$

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# Gauge invariance

$$\tilde{\Psi} = \Psi e^{i\kappa\chi}, \quad \tilde{\mathbf{A}} = \mathbf{A} + \nabla\chi, \quad \tilde{\Phi} = \Phi - \frac{\partial\chi}{\partial t}$$

Zero electric field potential gauge

$$\tilde{\Phi} = 0$$

$$\frac{\partial\chi}{\partial t} = \Phi$$